

Universal Shape Replicators via Self-Assembly with Attractive and Repulsive Forces^{*,†}

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Abstract

We show how to design a universal *shape replicator* in a self-assembly system with both attractive and repulsive forces. More precisely, we show that there is a universal set of constant-size objects that, when added to *any unknown* hole-free polyomino shape, produces an unbounded number of copies of that shape (plus constant-size garbage objects). The constant-size objects can be easily constructed from a constant number of individual tile types using a constant number of preprocessing self-assembly steps. Our construction uses the well-studied 2-Handed Assembly Model (2HAM) of tile self-assembly, in the simple model where glues interact only with identical glues, allowing glue strengths that are either positive (attractive) or negative (repulsive), and constant temperature (required glue strength for parts to hold together). We also require that the given shape has specified glue types on its surface, and that the feature size (smallest distance between nonincident edges) is bounded below by a constant. Shape replication necessarily requires a self-assembly model where parts can both attach and detach, and this construction is the first to do so using the natural model of negative/repulsive glues (also studied before for other problems such as fuel-efficient computation); previous replication constructions require more powerful global operations such as an “enzyme” that destroys a subset of the tile types.

1 Introduction

How can we harness the power of self-assembly to build a system that first senses the shape of a given unknown object, then builds copies of that shape, like the nanoscale equivalent of a photocopier? Although replicators are traditionally the subject of science fiction [15], biological reproduction illustrates that this is possible (at least approximately) in

the real world, and recent biological engineering shows that information can be replicated using DNA crystal growth and scission [13]. In this paper, we investigate more complex replication of *geometric shape*, using biologically realistic models (taken to an extreme admittedly not yet practical). To do so, we need a sufficiently flexible algorithmic model of self-assembly, and a replication “algorithm” defined by particles that interact with each other and the given object.

The standard algorithmic abstraction of self-assembly is to model the self-assembling particles as *Wang tiles*, that is, unit squares with a specified “glue” on each side, which can translate but not rotate; each glue has a nonnegative integer *strength*. In the *2-Handed Assembly Model* (2HAM), two assemblies (eventually) join together if they can be translated so as to match up glues of total strength at least τ , the *temperature* of the system. The resulting *terminal* assemblies are those that do not join into any other assemblies.

We can define the *replication problem* in this model: given an unknown initial assembly of tiles, design a collection of tiles or small assemblies to add to the self-assembly system such that the resulting terminal assemblies consist of copies of the given shape (plus possibly some small “trash” assemblies). However, this goal is impossible to achieve in just the 2HAM model, or any model with just a mechanism to join assemblies together: to sense a shape without destroying it, we need to be also able to split assemblies back apart.

The first extension of the 2HAM shown to enable a solution to the replication problem is the *RNAse enzyme* staged assembly model [1]. In this model, tiles can be of two types (DNA or RNA), the given shape is all one type (DNA), and there is an operation that destroys all tiles of the other type (RNA). Abel et al. [1] show that this model enables making a desired number k of copies of a given unknown hole-free shape or, through a complicated construction, infinitely many copies of the shape using just a constant number of tiles and stages. This result requires that the shape has a *feature size* (minimum distance between two nonincident edges) of $\Omega(\lg n)$ where n is the (unknown) number of tiles in the shape. The model is unsatisfying, however, in the way that it requires multiple stages and a global operation that modifies all tiles.

Another extension of the 2HAM shown to enable a partial solution to the replication problem is the *Signal Tile Assembly*

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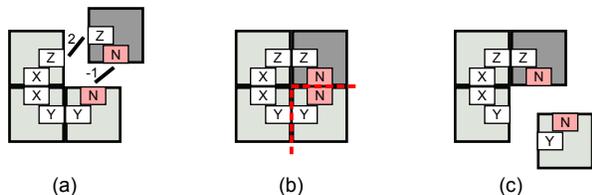


Figure 1: A simple example of attachment and detachment events and the notation for our constructions. On each tile, the glue label is presented. Red (shaded) labels represent negative glues, and the relevant glue strengths for the tiles can be found in the captions. For caption brevity, for a glue type X we denote $str(X)$ simply as X (e.g. $X + Y \implies str(X) + str(Y)$). In this temperature one, ($\tau = 1$) example, $X = 2$, $Y = 1$, $Z = 2$, and $N = -1$. (a) The three tile assembly on the left attaches with the single tile with strength $Z + N = 2 - 1 = \tau$ resulting in the 2×2 assembly shown in (b). However, this 2×2 assembly is unstable along the cut shown by the dotted line, since $Y + N = 1 - 1 < \tau$. Then the assembly is breakable into the assemblies shown in (c). Unlike Wang tilings, tiles with non-matching glues can be adjacent in this model; they simply contribute no strength.

Model (STAM) [7]. This powerful model allows tiles to change their glues and trigger assembly/disassembly events when tiles attach to other tiles. Keenan et al. [7] show that this model enables replicating a given unknown *pattern* of tiles in a rectangular shape, but not an arbitrary shape. Hendricks et al. [6] show that this model enables infinitely replicating a given unknown hole-free shape of feature size at least 2. The model is unsatisfying, however, in the way that it allows tiles to have arbitrarily complex behaviors. (Recent results show how to simulate part of STAM using 2HAM (in 3D) [5], but this simulation necessarily cannot simulate the necessary aspect of breaking assemblies apart.)

In this paper, we study a simple extension of 2HAM to allow glues of negative strength, that is, repulsive forces in addition to standard attractive forces. This extension is practical, as biology implements both types of forces [11], and well-studied theoretically: negative glues have already been shown to enable fuel-efficient computation [14], space-efficient computation [4], and computation even at temperature $\tau = 1$ [8, 9]. The complexity of combinatorial optimization problems with negative glues has also been studied [10]. We show that shape replication is possible in this model: adding a fixed constant number of constant-size assemblies to a given unknown hole-free shape results in terminal assemblies of infinitely many copies of that shape, plus constant-size trash assemblies.

2 Definitions and Model

Here we define the two-handed tile self-assembly model (2HAM) with negative and positive strength glue types, and formulate the problem of designing a tile assembly system that replicates any input shape. The 2HAM model was first

presented in [2]. The 2HAM is a variant of the abstract tile self-assembly model (aTAM) first presented in [12] in which there is no seed tile, and large assemblies may combine.

2.1 Tile Self-Assembly Model Tiles and Assemblies. A tile is an axis-aligned unit square centered at a point in \mathbb{Z}^2 , where each edge is labeled by a *glue* selected from a glue set Π . A *strength function* $str : \Pi \rightarrow \mathbb{Z}$ denotes the *strength* of each glue. Two tiles that are equal up to translation have the same *type*. A *positioned shape* is any *connected* subset of \mathbb{Z}^2 . Here, connected means for each (x, y) in the shape, at least one of $(x \pm 1, y)$ or $(x, y \pm 1)$ is also in the shape. A *positioned assembly* is a set of tiles at unique coordinates in \mathbb{Z}^2 , and the positioned shape of a positioned assembly A is the set of coordinates of those tiles.

For a given positioned assembly Υ , define the *bond graph* G_Υ to be the weighted grid graph in which each element of Υ is a vertex and the weight of an edge between tiles is the strength of the matching coincident glues or 0.¹ A positioned assembly C is said to be τ -*stable* for positive integer τ provided the bond graph G_C has min-cut at least τ , and C is said to be *connected* if every pair of vertices in G_C has a connecting path using only positive strength edges.

For a positioned assembly A and integer vector $\vec{v} = (v_1, v_2)$, let $A_{\vec{v}}$ denote the assembly obtained by translating each tile in A by vector \vec{v} . An *assembly* is a set of all translations $A_{\vec{v}}$ of a positioned assembly A . An assembly is τ -stable if and only if its positioned elements are τ -stable. An assembly is *connected* if its positioned elements are connected. A *shape* is the set of all integer translations for some subset of \mathbb{Z}^2 , and the shape of an assembly A is defined to be the union of the positioned shapes of all positioned assemblies in A . The *size* of either an assembly or shape X , denoted as $|X|$, refers to the number of elements of any positioned element of X .

Breakable Assemblies. An assembly is τ -*breakable* if it can be cut into two pieces along a cut whose strength sums to less than τ . Formally, an assembly C is *breakable* into assemblies A and B if A and B are connected, and the bond graph $G_{C'}$ for some assembly $C' \in C$ has a cut (A', B') for $A' \in A$ and $B' \in B$ of strength less than τ . We call A and B a pair of *pieces* of the breakable assembly C .

Combinable Assemblies. Two assemblies are τ -*combinable* provided they may attach along a border whose strength sums to at least τ . Formally, two assemblies A and B are τ -*combinable* into an assembly C provided $G_{C'}$ for any $C' \in C$ has a cut (A', B') of strength at least τ for some $A' \in A$ and $B' \in B$. We call C a *combination* of A and B .

Note that A and B may be combinable into an assembly that is not stable. This is a key property that is leveraged

¹Note that only matching glues of the same type contribute a non-zero weight, whereas non-equal glues always contribute zero weight to the bond graph. Relaxing this restriction has been considered as well [3].

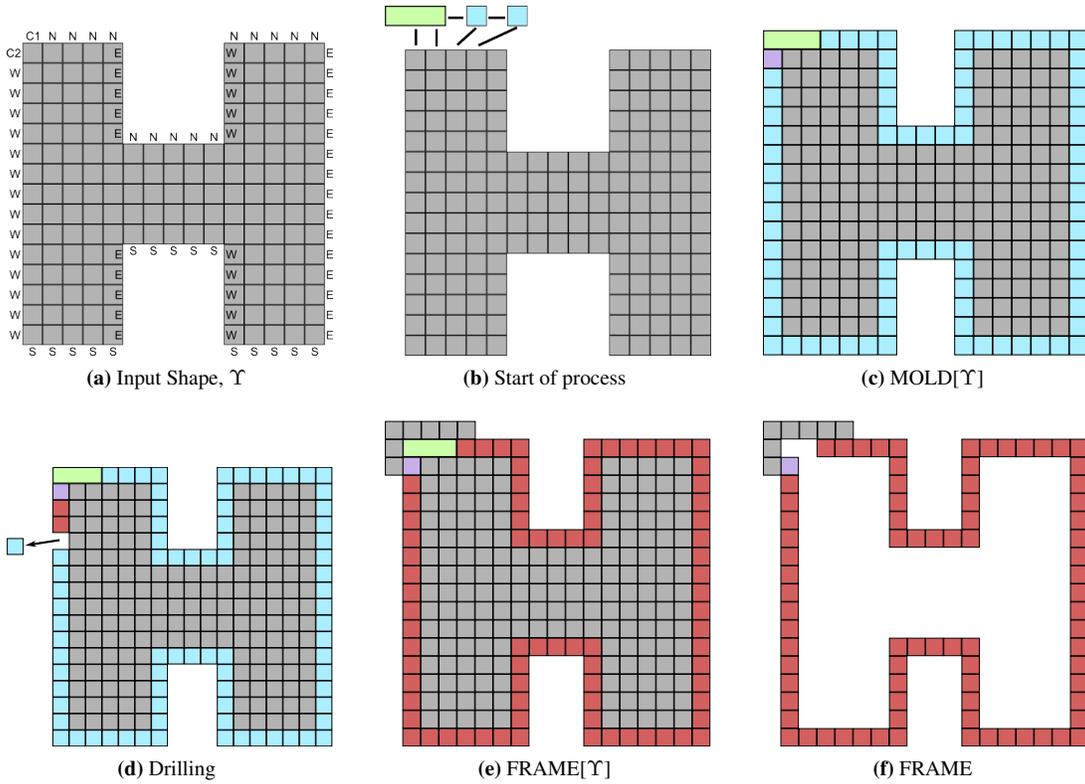


Figure 2: High level process for making the FRAME from input shape Υ .

throughout our constructions. See Figure 1 for an example.

States, Tile Systems, and Assembly Sequences. A *state* is a multiset of assemblies whose counts are in $Z^+ \cup \infty$. We use notation $S(x)$ to denote the multiplicity of an assembly x in a state S . A state S_1 *transitions* to a state S_2 at temperature τ , and is written as $S_1 \rightarrow_1^\tau S_2$, if S_2 is obtained from S_1 by either replacing a pair of combinable assemblies in S_1 with their combination assembly, or by replacing a breakable assembly in S_1 by its pieces. We simplify this to $S_1 \rightarrow_1 S_2$ when τ is clear from context. We write $S \rightarrow^\tau S'$ to denote the transitive closure of \rightarrow_1^τ , i.e., $S \rightarrow^\tau S'$ means that $S \rightarrow_1^\tau S_1 \rightarrow_1^\tau S_2 \rightarrow_1^\tau \dots S_k \rightarrow_1^\tau S'$ for some sequence of states $\langle S_1, \dots, S_k \rangle$.

A *tile system* is an ordered tuple $\Gamma = (\sigma, \tau)$ where σ is a state called the *initial system state* and τ is a positive integer called the *temperature*. We refer to any sequence of states $\langle \sigma, S_1, S_2, \dots, S_k \rangle$ such that $\sigma \rightarrow_1^\tau S_1$, and $S_i \rightarrow_1^\tau S_{i+1}$ for $i = \{1 \dots k-1\}$, as a *valid assembly sequence* for Γ . We denote any state P at the end of a valid assembly sequence (equivalently, $\sigma \rightarrow^\tau P$) as a *producible state* of Γ , and any assembly contained in a producible state is said to be a *producible assembly*. A producible state T is said to be *terminal* if T does not transition at temperature τ to any other state. A producible assembly is *terminal* if it is not breakable and not combinable with any other producible assembly.

2.2 Shape Replication Systems A system $\Gamma = (\sigma, \tau)$ is a *universal shape replicator* for a class of shapes if for any shape X in the class, there exists an assembly Υ of shape X such that system $\Gamma' = (\sigma \cup \Upsilon, \tau)$ (i.e., Γ with a single copy of Υ added to the initial state) produces an unbounded number of assemblies of shape X , and essentially nothing else. We formalize this in the following definition, and then add some discussion of additional desirable properties a replicator might have.

DEFINITION 2.1. (UNIVERSAL SHAPE REPLICATOR) A system $\Gamma = (\sigma, \tau)$ is a *universal shape replicator* for a class of shapes U if for any shape $X \in U$, there exists an assembly Υ of shape X such that system $\Gamma' = (\sigma \cup \Upsilon, \tau)$ has the following properties:

- For any positive integer n and producible state S , there exists a producible state S' containing at least n terminal assemblies of shape X such that $S \rightarrow^\tau S'$.
- All terminal assemblies of super-constant size have shape X .

In addition to the above replicator properties, there are some additional desirable properties a universal replicator might have. For example, the producible assemblies of the system should be limited in size as much as possible

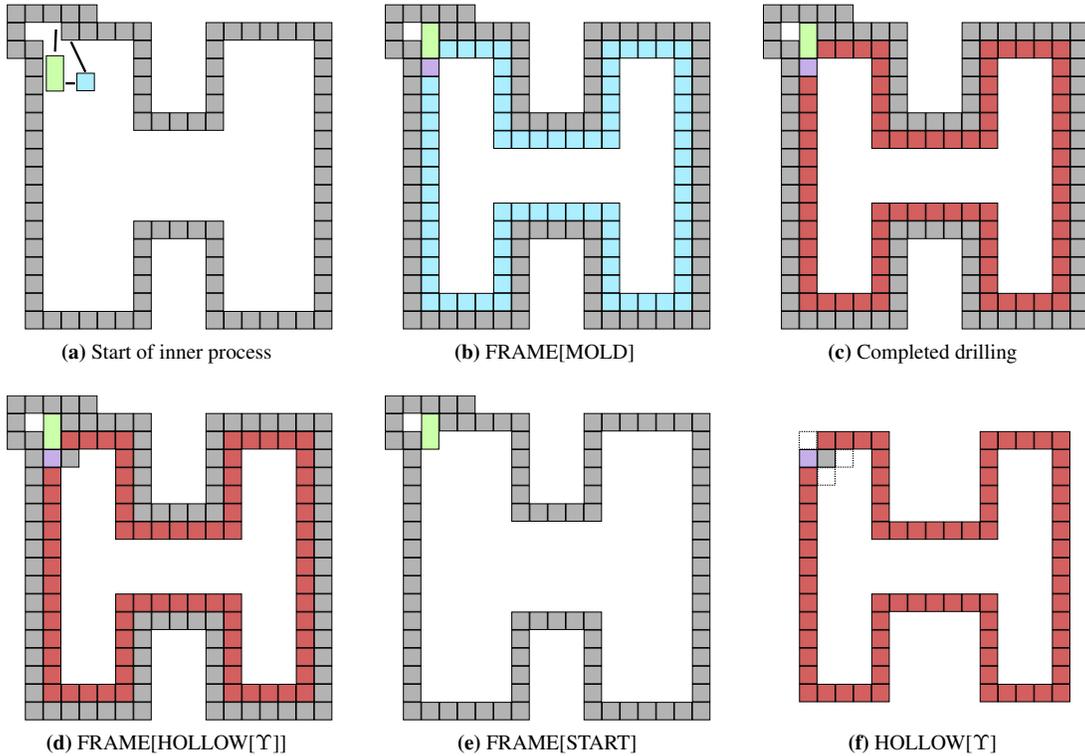


Figure 3: High level process for making a copy of an input shape Υ from a *frame* of Υ .

($O(|X|)$ in the best possible case). Additionally, it may be desirable to place substantial limitations on the complexity of the initial input assembly Υ , e.g., require its surface to expose essentially a single type of glue for each edge orientation. Our universal replicator achieves the following *bonus* constraints.

DEFINITION 2.2. (BONUS PROPERTIES!) A universal replicator is said to be *sleek* if it has the following properties:

- (bonus!) All producible assemblies have size $O(|X|)$.
- (bonus!) The input assembly Υ is rather simple: on the exposed surface of the assembly, a single glue type is exposed for each edge orientation (e.g. *North*, *East*, *South*, and *West*), with at most $O(1)$ *special* tiles violating this convention. Additionally, any non-surface glues (glues which bind the shape together) must have sufficiently large strength so that no cuts can be made through the shape when negative glues are introduced, but otherwise have no constraints.

The class of shapes which can be replicated by the system described in this paper are hole-free polyominoes with *feature size* of at least 9. The feature size of a shape is defined as follows (we use the same definition as [1]): for two points a, b in the shape, let $d(a, b) = \max(|a_x - b_x|, |a_y - b_y|)$. Then the feature size is the minimum $d(a, b)$ such that a, b are on two non-adjacent edges of the shape (edges which do not

share a vertex). The feature size ensures that the replication gadgets ($O(1)$ sized assemblies used to replicate the shape) function properly (e.g. the gadgets can encompass the shape without “bumping into” each other). Formally, we prove the following:

THEOREM 2.1. *There exists a sleek universal shape replicator $\Gamma = (\sigma, 10)$ for genus-0 (hole-free) shapes with feature size of at least 9.*

3 Overview of Replication Process

The high-level process for replicating a given input assembly Υ is described here. We assume that Υ has special glues along its perimeter such that all North, East, South, and West facing edges have glues of N , E , S , and W , respectively, with the exception of the Northernmost-Westernmost unit of the shape having a North glue of $C1$ and West glue of $C2$ (Fig. 2a). Intuitively, the process is to assemble an outline of Υ that is filled to have the same shape as Υ . In Phase 1, *mold gadgets* attach clockwise along the outside perimeter of Υ , to detect the edges of the shape. In Phase 2, the mold gadgets are replaced, counterclockwise gadget-by-gadget, by *drill gadgets*. These drill gadgets follow the path laid out by the mold gadgets and do not attach to the shape. The drill gadgets use negative glues to destabilize adjacent mold gadgets. This technique is used to create an assembly called the FRAME

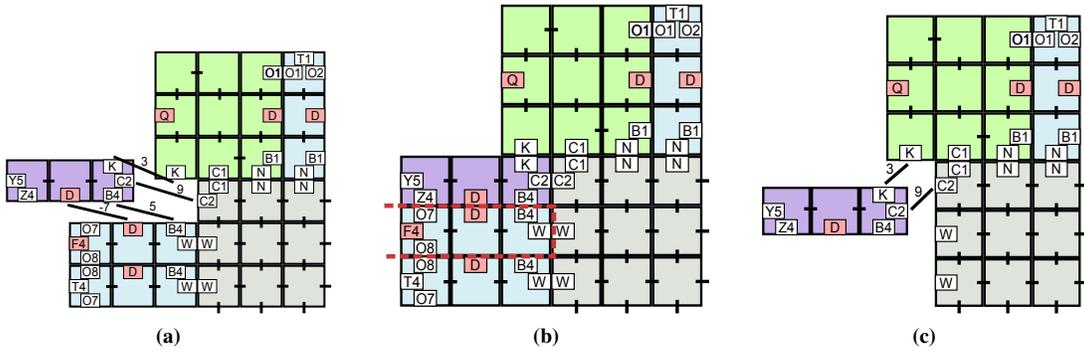


Figure 5: The pre-drill process. (a) Case 1: The mold process has completed. The pre-drill gadget attaches cooperatively to the start gadget, input shape, and a mold gadget. $K + C2 + B4 + D = 3 + 9 + 5 - 7 \geq \tau$. (b) The pre-drill gadget destabilizes the adjacent mold gadget. $B4 + W + O8 + D = 5 + 9 + 1 - 7 < \tau$. (c) Case 2: The mold process has not completed, the pre-drill gadget may still attach. After attachment, the negative ‘D’ glue prevents a mold gadget from occupying the space directly below. $K + C2 = 3 + 9 \geq \tau$.

Label	Str	Label	Str
C1	2	C2	9
N,E,S,W,n,e,s,w	9	T*,t*,O*,o*,L	1
B*,b*	5	K,k	3
X*,Y*,Z*,x*,y*,z*	9	D	-7
F*,f*	-2	V*,U*,H*,J*,S*,v*,u*,h*,j*,s*	9
R,r	2	A*	10
g*	9	M*	5
Q	-2	q	-5

Table 1: The glue strengths (Str) of each glue label (Label) in the replication system.

replication system. These gadgets are designed to work in a temperature $\tau = 10$ system. There is a constant number of these distinct gadget types which are used to replicate arbitrarily sized input assemblies. In our figures, a black line perpendicular and in the middle of the edge of two adjacent tiles indicates a unique infinite strength bond (i.e. the strength of the glue is $\gg \tau$ such that no detachment events can occur in which these tiles are separated). Although each glue strength can be found in the figures and their captions, there is a full table of glue strengths in Table 1. First, we describe the gadgets used in the process of creating the layer of mold gadgets around the outer perimeter of the input assembly.

4.1 Phase 1 Gadgets for the Outer Mold

Below we describe the gadgets used to implement Phase 1 and create MOLD[Υ].

Start gadget. The start gadget is an assembly, designed to attach using the C1 glue and N glue, which designates the Northernmost-Westernmost corner of the input assembly. Once the start gadget attaches, a North mold gadget may attach (Fig. 4a).

Mold gadgets. The mold gadgets, beginning at the start gadget as shown in Figure 4a, walk along the input

assembly in a clockwise manner to create MOLD[Υ]. The North (South) mold gadgets are 1×3 assemblies designed to walk from West to East (East to West) along the North (South) edges of the input assembly. The West (East) mold gadgets are 3×1 assemblies designed to walk from South to North (North to South) along the West (East) edges of the input assembly. The mold gadgets expose either a positive or negative glue on their unused edge (e.g. North mold gadgets expose either a T1 or F1) used for detecting corners and drilling at corners, respectively.

Corner mold gadgets. The *corner mold gadgets* attach at corners of the input assembly once a mold gadget has reached the corner. Two sets of corner mold gadgets are used; one for concave corners and one for convex corners. There are two types of concave and convex corner mold gadgets. This is due to the edge length being even or odd. If the mold gadget that places adjacent to a corner of the shape has two negative glues, we denote the concave corner as a *type-1* concave corner and otherwise as a *type-2* concave corner. A type-1 concave corner gadget attachment can be seen in Figure 4b, and convex in Figure 4c. Type-2 corner gadget details can be seen in Figure 4. The North \rightarrow West (South \rightarrow East) corner gadget attaches cooperatively to a North (South) mold gadget and the input shape. The East \rightarrow North (West \rightarrow South) corner gadget attaches cooperatively to a East (West) mold gadget and the input shape.

4.2 Phase 2 Gadgets for Making the FRAME

Below we describe the gadgets used to implement Phase 2 and create FRAME and START[Υ].

Pre-drill gadget. A gadget that binds to the start gadget, a mold gadget (in some cases), and the input shape that is designed to allow the placement of a *West drill helper* to its South. It allows the drilling process to begin once mold gadgets have finished encircling the input shape (Fig. 5).

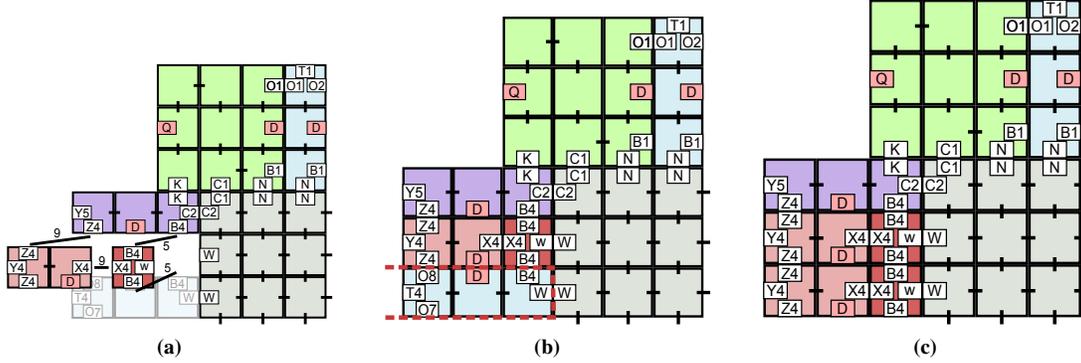


Figure 6: The drilling process begins. (a) A West drill helper attaches cooperatively to the pre-drill gadget and a mold gadget. $B4 + B4 = 5 + 5 \geq \tau$. A drill gadget attaches cooperatively to the pre-drill gadget and drill helper. $Z4 + X4 + D = 9 + 9 - 7 \geq \tau$. (b) The drill gadget destabilizes the mold gadget underneath. $B4 + W + O7 + D = 5 + 9 + 1 - 7 < \tau$. (c) The removal of the mold gadget allows the process shown in (a) and (b) to repeat. The process continues along the face of the shape.

Drill gadgets. The drill gadgets (Fig. 6a), along with drill helpers, walk along the boundary of the input assembly in a counter-clockwise manner destabilizing mold gadgets and replacing them to create the FRAME. The drill gadgets do not attach to the input shape Υ , so when the drills have removed all of the mold gadgets, the FRAME will not be attached to the input shape. The drill gadgets are assemblies that attach to the North (South) drill helpers and destabilize mold gadgets to their East (West). The West (East) drill gadgets are assemblies that attach to the West (East) drill helpers and destabilize mold gadgets to their North (South).

Drill helpers. The drill helpers (Fig. 6a) are 1×1 assemblies that, beginning at the pre-drill gadget, walk along the boundary of the input assembly in a counter-clockwise manner exposing glues that allow drill gadgets to destabilize adjacent mold gadgets. These gadgets walk along the boundary by following glues exposed by mold gadgets, rather than using glues on the input assembly.

Drill corner gadgets. Drill corner gadgets bind cooperatively at type-1 and type-2 corners to drill helpers and mold gadgets in order for the drilling process to turn corners. Details can be seen in Figures 7,8,and 9.

Post-drill gadget. *Post-drilling* refers to the the process of removing the input shape to create a FRAME. It is needed because the pre-drill gadget is still attached to the input shape. The post-drill gadget may attach once the drill gadgets have encircled the input shape. It attaches to the pre-drill gadget and last-placed drill gadget. Once attached, it destabilizes the assembly with the input shape and start gadget to create the FRAME. (See Fig. 10.)

4.3 Phase 3 Gadgets for the Inner Mold Here we describe the gadgets used to implement Phase 3 and create FRAME[MOLD]. The *inner mold gadgets* are similar to the mold gadgets used in Section 4.1, with changes to allow them

to encircle the inside perimeter of the FRAME, rather than the outside perimeter of the input shape Υ . The Phase 3 gadgets (shown in Figure 11) include an *inner start gadget* which attaches to the FRAME to allow the attachment of inner mold gadgets which attach along the inside perimeter of the FRAME in a clockwise manner. The inner mold gadgets reflect the form and function of the mold gadgets shown in Section 4.1, handling corners in a similar way. Type-2 inner mold corner gadgets can be seen in Figures 11(d-e).

4.4 Phase 4 Gadgets for Making the Hollow Outline

Below we describe the gadgets used to implement Phase 4 and create FRAME[START] and HOLLOW[Υ]. The *inner pre-drill gadget* can attach to the FRAME after the inner start gadget has placed, similar to the pre-drill gadget shown in Section 4.2. The inner pre-drill gadget can be seen in Figure 12. Once the inner pre-drilling gadget has attached, the inner drill gadgets attach along the inside edge of the frame, removing the inner mold gadgets one by one counterclockwise. These gadgets reflect the form and function of the drill gadgets shown in Section 4.2. The inner drilling process reflects that of the outer drilling, and can be seen in Figure 13a. Corners are handled similarly to the *outer* drill gadgets, from Phase 2 (Section 4.2) An. When the drills completely attach to the inner perimeter of the FRAME, the *inner post-drill gadget* can attach, as seen in Figure 14a, to create FRAME[HOLLOW[Υ]]. After the inner post-drill gadget attaches, the assembly destabilizes into FRAME[START] and HOLLOW[Υ], as shown in Figure 14b.

4.5 Phase 5 Gadgets to Fill the Hollow Outline

Below we describe the gadgets used to implement Phase 5 to fill HOLLOW[Υ] to create COPY[Υ]. The *filler gadgets* begin the process of filling the shape, shown in Figure 15. Two regions of HOLLOW[Υ] need to be filled to become COPY[Υ],

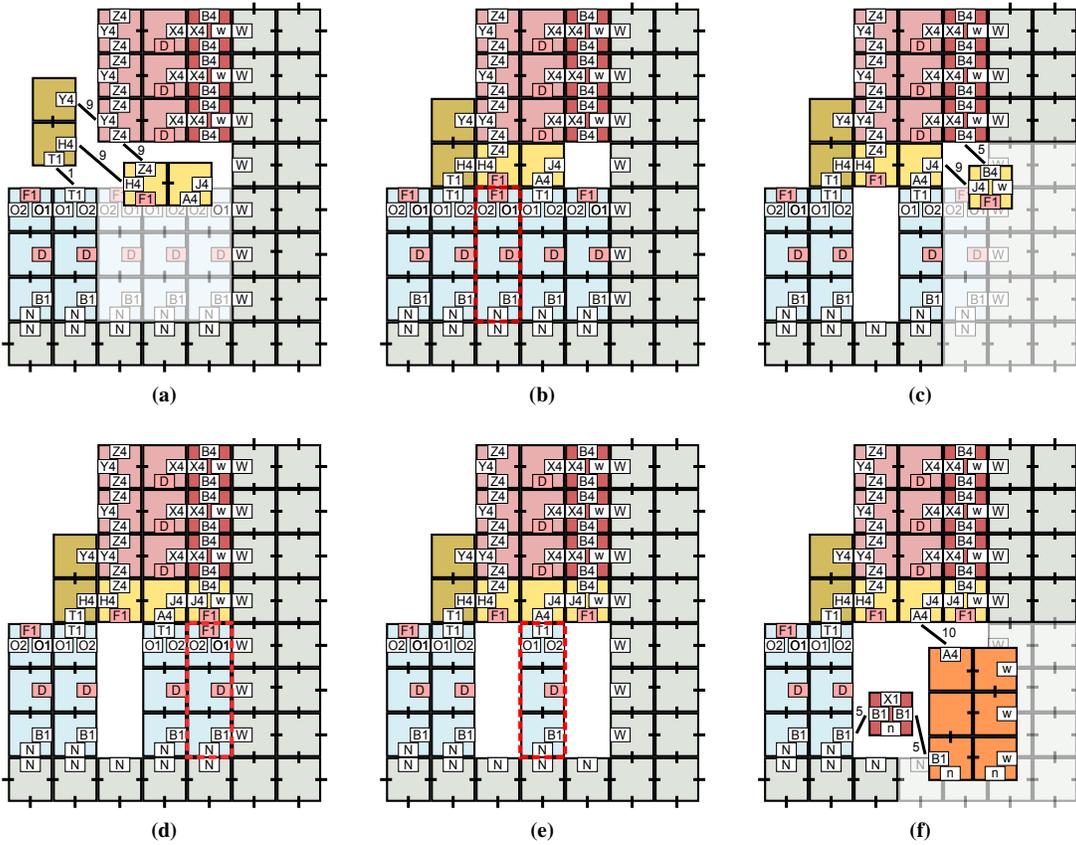


Figure 7: The drilling process encounters a type-1 concave corner of the assembly. (a) A drill gadget destabilizes the North→West corner gadget. $B4 + W + T1 + D = 5 + 9 + 1 - 7 < \tau$. A West→North drill corner helper attaches to a mold gadget and a drill gadget. $Y4 + T1 = 9 + 1 \geq \tau$. A West→North drill corner gadget attaches, cooperatively. $H4 + Z4 + F1 = 9 + 9 - 2 \geq \tau$. (b) The West→North drill corner gadget destabilizes a mold gadget to its South. $O1 + N + O2 + F1 = 1 + 9 + 1 - 2 < \tau$. (c) A mold gadget has destabilized and has broken off the assembly. Another West→drill gadget attaches. (d) destabilizes a mold gadget to its South. $N + O2 + F1 = 9 + 1 - 2 < \tau$ (e) Without any adjacent mold gadgets to its East or West, a mold gadget becomes unstable. $N = 9 < \tau$. (f) A drill corner gadget fills in the space in the concave corner and exposes a glue that will allow drilling to continue to the West. $A4 = 10 \geq \tau$.

the Northernmost-Westernmost corner (Figure 15a) and the interior (Figures 15b,15c).

4.6 Temperature and Minimum Feature Size In this section we discuss the temperature used in the construction and the minimum feature size required by the input shape to be replicated. In Table 2, a set of inequalities related to glue strengths and temperature is listed. These inequalities must be satisfied for the attachment and detachment events to occur as in the sections described above. Although minimizing temperature was not a goal of this work, this set of inequalities can be used to find a minimum working temperature for this system. Additionally, as minimizing temperature was not considered, there may be changes to the design of the gadgets used which further reduce the temperature below what is implied by the inequalities. The gadgets, as designed, require

the input shape to have minimum feature size 9. Particularly, given an input shape with smaller minimum feature size, the inner mold process may have *overlapping* problems when the topmost-leftmost area of the FRAME has two *tight* corners. If the two non-adjacent edges on which two points have distance less than 9 occurs at the top-left of the input shape, we consider the final filling process shown in Section 4.5. The blue tiles shown in Figure 15 cannot be placed as the drill gadgets protruding eastward from the FRAME will have already attached. As this is the only problem area, feature sizes across the rest of the input shape may be smaller than 9 and still succeed in replication, but this is not considered closely or formally shown; we constrain the input shape to have minimum feature size 9.

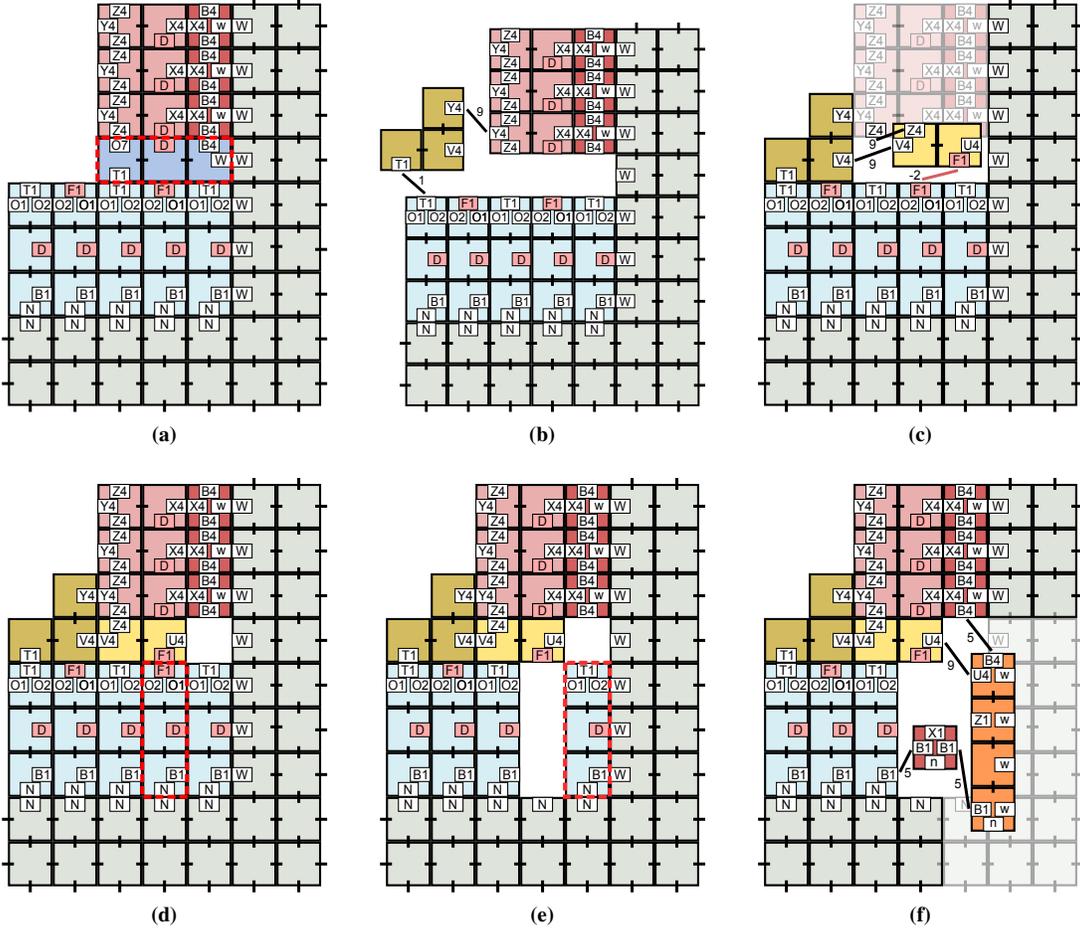


Figure 8: The drilling process encounters a type-2 concave corner of the assembly. (a) A drill gadget destabilizes the North→West corner gadget. $B4 + W + T1 + D = 5 + 9 + 1 - 7 < \tau$ (b) A West→North drill corner helper attaches to a mold gadget and a drill gadget. $Y4 + T1 = 9 + 1 \geq \tau$. (c) A West→North drill corner gadget attaches, cooperatively. $V4 + Z4 + F1 = 9 + 9 - 2 \geq \tau$. (d) The West→North drill corner gadget destabilizes a mold gadget to its South. $O1 + N + O2 + F1 = 1 + 9 + 1 - 2 < \tau$. (e) Without a mold gadget to its West, the mold gadget in the concave corner is unstable. $N = 9 < \tau$. (f) A drill corner gadget fills in the space in the concave corner. $U4 + B4 = 9 + 5 \geq \tau$. This gadget exposes a glue on its West side that allows drilling to continue to the West. $B1 + B1 = 5 + 5 \geq \tau$.

5 Universal Shape Replication

In this section we formally state the results, including the class of shapes which can be replicated by the replication gadgets discussed in the previous section. The input shape must be sufficiently large for the replication gadgets to assemble in the intended manner, so we define the *feature size* of a shape as follows (we use the same definition as [1]): for two points a, b in the shape, let $d(a, b) = \max(|a_x - b_x|, |a_y - b_y|)$. Then the feature size is the minimum $d(a, b)$ such that a, b are on two non-adjacent edges of the shape.

THEOREM 5.1. *There exists a sleek universal shape replicator $\Gamma = (\sigma, 10)$ for genus-0 (hole-free) shapes with feature size of at least 9.*

Proof. The proof follows by constructing an unbounded shape replication system $\Gamma = (\sigma, 10)$. Consider an initial assembly state σ consisting of infinite counts of the tiles which construct the replication gadgets shown in Section 4. For any shape X of genus-0 and minimum feature size 9, consider an assembly Υ of shape X with the properties discussed at the beginning of Section 4 (i.e., the exposed glues on Υ are $N, E, S,$ and W based on edge orientation, and there is a special glue in the Northernmost-Westernmost position of Υ which exposes glues $C1$ to the North and $C2$ to the West). Then we prove inductively that $\Gamma' = (\sigma \cup \Upsilon, 10)$ has the following property: for any $n \in \mathbb{N}$ and producible state S of Γ' , there exists a producible state S' containing at least n terminal assemblies of shape X such that $S \rightarrow S'$.

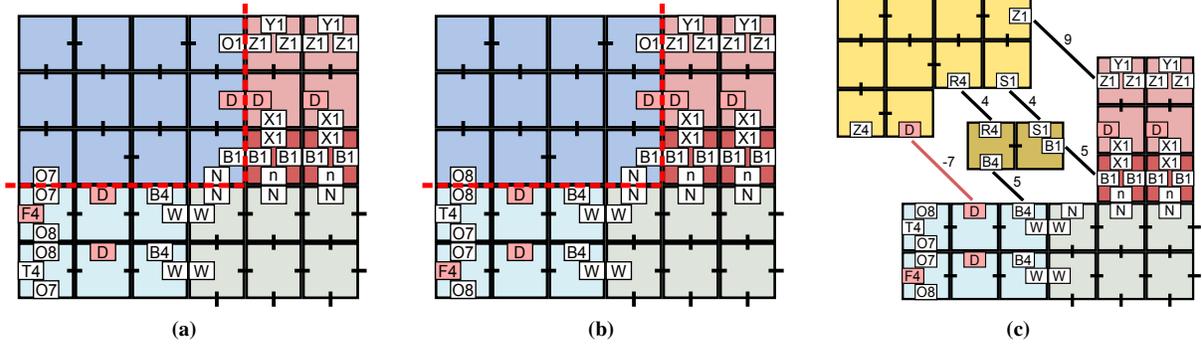


Figure 9: The drilling process encounters convex corners of the assembly. (a) Coming from the East, drill gadgets encounter a type-1 convex corner of the assembly. The mold corner gadget becomes unstable and will break from the assembly. $O7 + N + B1 + D = 1 + 9 + 5 - 7 \geq \tau$. (b) The drill gadgets encounter a type-2 convex corner gadget. It becomes unstable and will break from the assembly. $O8 + N + B1 + D = 1 + 9 + 5 - 7 < \tau$. (c) Convex corner gadgets bind and allow the drilling process to continue. $B4 + B1 = 5 + 5 \geq \tau$. $Z1 + R4 + S1 + D = 9 + 4 + 4 - 7 \geq \tau$.

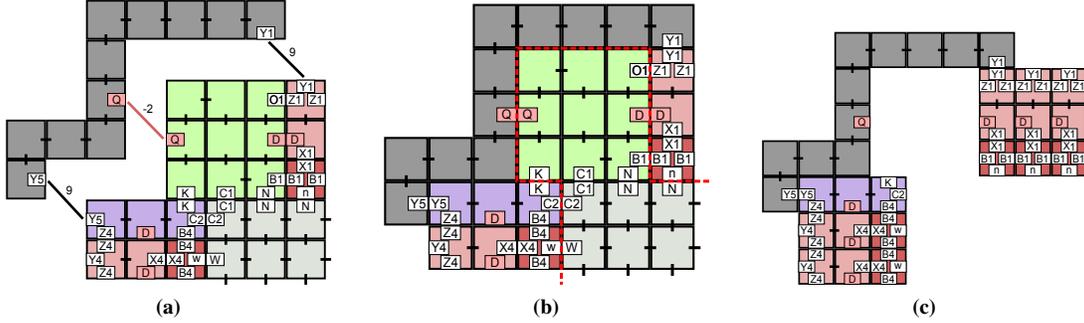


Figure 10: The post-drill process begins. (a) The post-drill gadget binds at the Northernmost-Westernmost corner of the assembly that contains the input shape. It binds cooperatively to the last placed drill block and the pre-drill gadget. $Y5 + Y1 + Q = 9 + 9 - 2 \geq \tau$. (b) Once placed, the pre-drill gadget destabilizes a cut which includes the input shape and the start block. $B1 + C2 + K + Q + D = 5 + 9 + 3 - 2 - 7 < \tau$. (c) Once the assembly with the input shape and the start block detaches, the FRAME remains.

For the base, note that the Γ' follows the process described in Section 4. When the FRAME detaches from $\text{HOLLOW}[\Upsilon]$, $\text{HOLLOW}[\Upsilon]$ is filled to generate 1 terminal assembly of shape X . Then, for any producible state S , $\sigma \cup \Upsilon \rightarrow S$ by definition, so S contains at least 1 terminal of shape X or $S \rightarrow \hat{S}$ such that \hat{S} contains at least 1 terminal of shape X .

Now, consider any producible state A such that A has at least $n \in \mathbb{N}$ terminal assemblies of shape X . For A to have at least one such terminal, $\text{HOLLOW}[\Upsilon]$ must have detached from the FRAME. When this occurs, the FRAME is still attached to the inner start gadget, so the inner mold/drill process repeats, generating $\text{HOLLOW}[\Upsilon]$. Again, $\text{HOLLOW}[\Upsilon]$ detaches from the FRAME, and then $\text{HOLLOW}[\Upsilon]$ is filled, resulting in 1 more terminal assembly of shape X . Therefore $A \rightarrow A'$ such that A' contains at least $n + 1$ terminal assemblies of shape X . Then, since S or \hat{S} contains at least 1 terminal of shape X , $S \rightarrow S'$ such that S'

has at least n terminal assemblies of shape X for any n . This satisfies the first property of Definition 2.1.

Further, any terminal assembly B in the system that does not have shape X , $|B| = \mathcal{O}(1)$, satisfying the second property of Definition 2.1. Note that the only assemblies which are larger than $\mathcal{O}(1)$ size are assemblies related to the input shape, the FRAME, and $\text{HOLLOW}[\Upsilon]$. The input shape and the intermediate assemblies produced while creating the FRAME are not terminal since the process repeats once the FRAME is detached. The FRAME and the intermediate assemblies produced while creating $\text{HOLLOW}[\Upsilon]$ are not terminal since the process repeats once $\text{HOLLOW}[\Upsilon]$ detaches. $\text{HOLLOW}[\Upsilon]$ fills to create a terminal assembly of shape X , so none of the intermediate assemblies are terminal.

Then, $\Gamma = (\sigma, 10)$ is a universal shape replicator for genus-0 (hole-free) shapes with minimum feature size 9. To show that it is a sleek universal shape replicator (i.e. the bonus properties discussed in the definitions apply), note

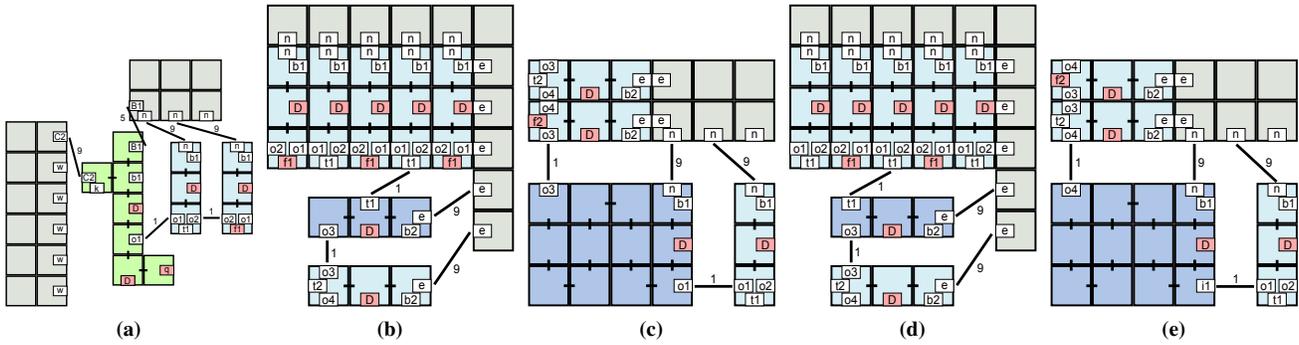


Figure 11: (a-c) Starting the inner mold process and handling type-1 corners. (a) The inner start gadget attaches to the inside perimeter of the FRAME. $C2 + B1 = 9 + 5 \geq \tau$. An inner mold gadget attaches cooperatively to the start gadget and the FRAME. $o1 + n = 1 + 9 \geq \tau$. Another inner mold gadget attaches cooperatively to the FRAME and the previous inner mold gadget. $o2 + n = 1 + 9 \geq \tau$. (b) A concave corner of the assembly. A South→West concave corner gadget attaches to the concave corner. $t1 + e = 1 + 9 \geq \tau$. An inner mold gadget attaches cooperatively to the FRAME and the South→West concave corner gadget. $o3 + e = 1 + 9 \geq \tau$. (c) A convex corner of the assembly. A West→South convex corner gadget attaches at the convex corner, allowing the mold process to continue around the convex corner. $o3 + n = 1 + 9 \geq \tau$. $o1 + n = 1 + 9 \geq \tau$. (d-e) Type-2 concave and convex corners of the assembly. (d) A type-2 South→West concave corner gadget binds, which allows the mold process to continue around the concave corner. $t1 + e = 1 + 9 \geq \tau$. $o3 + e = 1 + 9 \geq \tau$. (e) A type-2 West→South corner gadget binds allowing the mold process to continue around the convex corner. $o4 + n = 1 + 9 \geq \tau$. $o1 + n = 1 + 9 \geq \tau$.

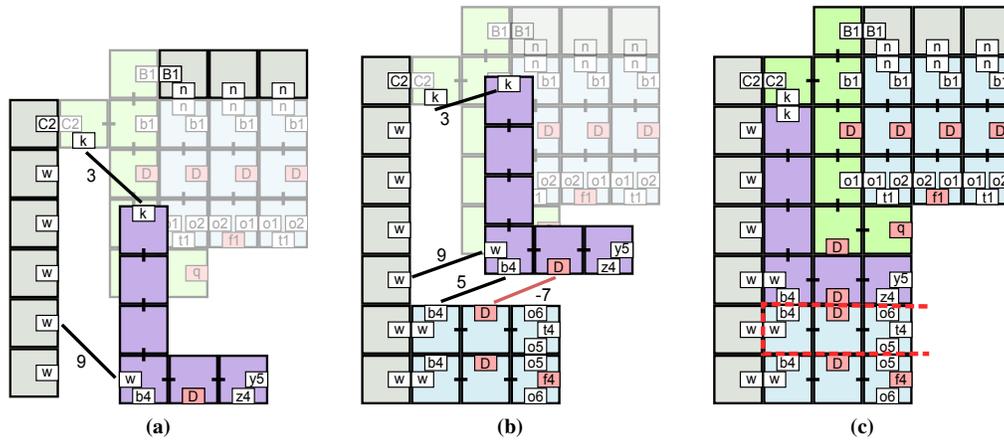


Figure 12: The inner pre-drilling process begins. (a) Case 1: The inner mold process has not completed and the inner pre-drill gadget binds cooperatively to the FRAME and the inner start gadget. $w + k = 9 + 3 \geq \tau$. (b) Case 2: The inner mold process has completed and the inner pre-drill gadget binds cooperatively to the FRAME, inner start gadget, and an inner mold gadget. $w + k + b4 + D = 9 + 3 + 5 - 7 \geq \tau$. (c) The inner pre-drill gadget prevents any inner mold gadget from attaching to its south and destabilizes any inner mold gadget that may have been in that space. $b4 + o5 + w + D = 5 + 1 + 9 - 7 < \tau$.

that the input shape considered here has the same properties as described in that definition, and that the input shape, the FRAME, HOLLOW[Υ], and the intermediate steps of each of these assemblies, do not grow larger than $\mathcal{O}(|X|)$ in size.

6 Conclusion

In this work we formally introduced the problem of shape replication in the 2-handed tile assembly model and provided a universal replication system for all genus-0 shapes with

at least a constant minimum feature size. Shape replication has been studied in more powerful self-assembly models such as the staged self-assembly model and the signal tile model. However, our result constitutes the first example of general shape replication in a passive model of self-assembly where no experimenter intervention is required, and where the system monomers are state-less, static pieces that interact based purely on the attraction and repulsion of surface chemistry.

Phase 1	
$C + N \geq \tau$	$O + N \geq \tau$
$T + W \geq \tau$	
Phase 2: Pre-drilling	
$K + C2 + B + D \geq \tau$	$K + C2 \geq \tau$
$B + W + O + D < \tau$	
Phase 2: Drilling	
$B + B \geq \tau$	$Z + X + D \geq \tau$
$B + X \geq \tau$	
Phase 2: Drilling Type-1 Corners	
$B + W + T + D < \tau$	$Y + T \geq \tau$
$Z + V + F \geq \tau$	$Y + Z + T + F \geq \tau$
$Z + B + V + Y + F \geq \tau$	$Z + X + V + Y + F \geq \tau$
$T + Z + B + F \geq \tau$	$O + N + O + F < \tau$
$B + B \geq \tau$	$B + U \geq \tau$
Phase 2: Drilling Type-2 Corners	
$Z + H + F \geq \tau$	$H + Y + Z + B + F \geq \tau$
$H + Y + Z + X + F \geq \tau$	$T + Z + B + F \geq \tau$
$O + N + O + F < \tau$	$N < \tau$
$A \geq \tau$	$B + B \geq \tau$
Phase 2: Drilling Obtuse Corners	
$B + N + O + D < \tau$	$B + B \geq \tau$
$Z + R + S + D \geq \tau$	$O + W + B + D < \tau$
Phase 2: Post-Drilling	
$B + N + C1 + K + D \geq \tau$	$Y + Y + Q \geq \tau$
$Y + Z + B + N + C1 + K + Q \geq \tau$	$B + N + C1 + C2 + B + Z + Y + Q + D \geq \tau$
$Y + Z + B + C2 + K + Q \geq \tau$	$B + N + C1 + K + D + Q \geq \tau$
$C2 + C1 + N \geq \tau$	$K + B + C2 + Q + D < \tau$
Phase 3	
$C2 + B \geq \tau$	$o + n \geq \tau$
$t + e \geq \tau$	
Phase 4 - Pre-drilling	
$k + w + b + D \geq \tau$	$b + w + i + D < \tau$
$k + w \geq \tau$	
Phase 4 - Drilling	
$b + b \geq \tau$	$z + x + D \geq \tau$
$b + w + i + D < \tau$	$b + x \geq \tau$
Phase 4 - Post-drilling	
$B + b + k + C2 + D \geq \tau$	$y + y + Q \geq \tau$
$B + b + k + C2 + D + Q \geq \tau$	$b + k + w + D + q < \tau$
$B + C2 \geq \tau$	$B + C2 + C1 + N + B1 + O + D \geq \tau$
$Z + B \geq \tau$	$B + W + W + O + D \geq \tau$
$k + y \geq \tau$	
Phase 5	
$L + g^* \geq \tau$	$M + M \geq \tau$

Table 2: Shown are the inequalities which must be satisfied for the replication gadgets shown in Section 4 to function in the way required to prove Theorem 5.1. All single glue labels except A must have strength $< \tau$. Unless otherwise stated, in these inequalities, a glue label G represents all glues G^* (e.g., $G1, G2$, etc.).

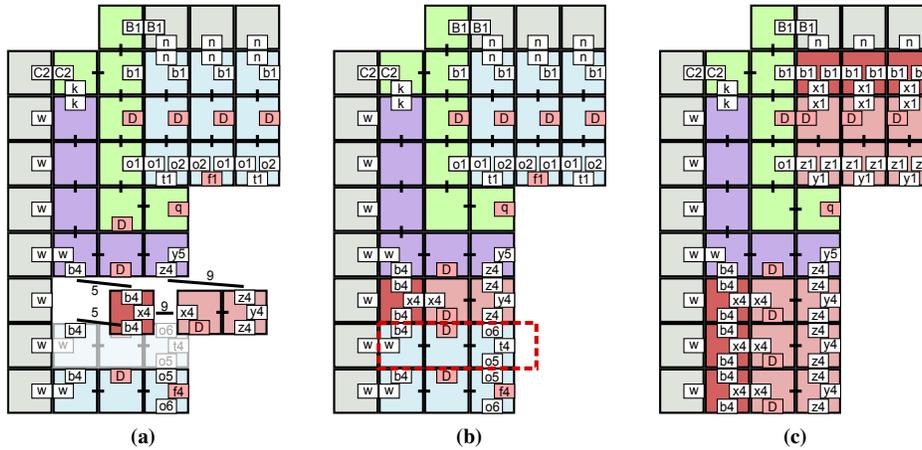


Figure 13: The inner drilling process begins. (a) A drill helper binds to the inner pre-drill gadget and an inner mold gadget. $b4 + b4 = 5 + 5 \geq \tau$. A drill block binds cooperatively to the drill helper and pre-drill gadget. $x4 + z4 + D = 9 + 9 - 7 \geq \tau$. (b) The drill gadgets destabilize an inner mold gadget. $b4 + o5 + w + D = 5 + 1 + 9 - 7 < \tau$. (c) The drilling process continues counter-clockwise along the inside perimeter of the FRAME until the drill gadgets reach the inner start gadget.

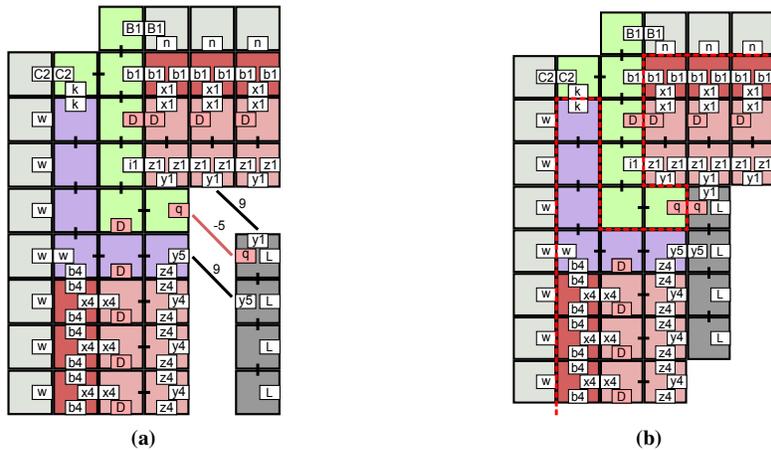


Figure 14: The inner post-drilling process. (a) The inner post-drill gadget binds cooperatively to the inner pre-drill gadget and the second-to-last placed drill gadget. $y5 + y1 + q = 9 + 9 - 5 \geq \tau$. (b) The assembly with the FRAME and the start gadget becomes unstable and breaks off the assembly. $b1 + w + k + q + D = 5 + 9 + 3 - 5 - 7 < \tau$.

Our work opens a number of directions for future work. One direction includes analyzing and improving the *rate* of replication. Under a reasonable model of replication time, our construction should constitute a *quadratic* replicator—in that after time t , $\Omega(t^2)$ copies of the input shape are expected. Designing a faster replicator is an open question. In particular, achieving an *exponential* replicator is an important goal. Further, to properly consider these questions requires a formal modelling of replication rates for this model.

Another direction is to further generalize the class of shapes that can be replicated. For example, can shapes with holes be replicated? This is likely difficult, but might be achievable by drilling into the input assembly in a carefully engineered way. Achieving such general replication would be the first example of shape replication that extends beyond

genus-0. This seems to require a shape with more complex glues, which leads to another area of research.

The consideration of variations of the *sleek* requirements may be of interest. For example, removing the need for any special tiles from the replication system might be achievable. Or, allowing for more complex input assemblies could allow for high genus replication, as discussed above. Finally, determining the lowest necessary temperature and glue strengths needed for replication is an open question. We use temperature value 10 to maximize clarity of the construction and have not attempted to optimize this value. To help such optimization, we have included a compiled table (Table 2) showing the inequality specifications induced by our construction for each gadget to help guide where a modification to the replication algorithm might reduce the

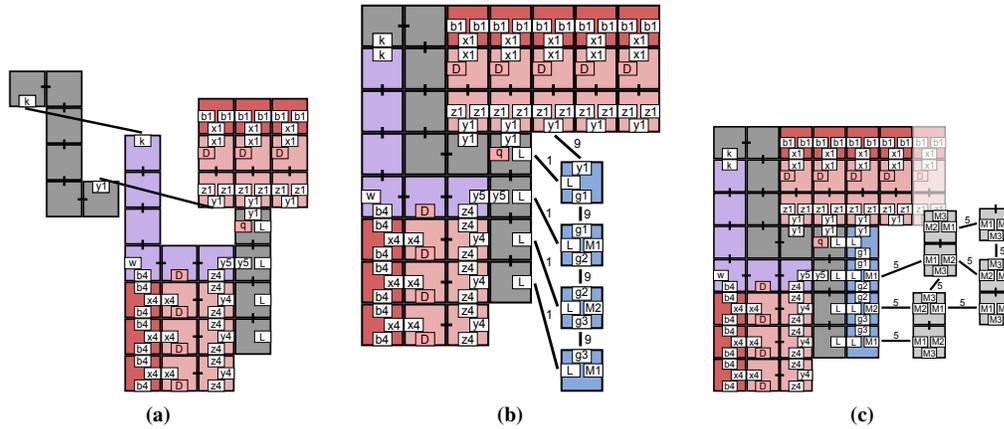


Figure 15: The inner filling process. (a) The first filler gadget comes in to fill in the Northernmost-Westernmost corner of HOLLOW[Υ]. $k + y1 = 3 + 9 \geq \tau$. (b) $L = 1, g^* = 9$. (c) $M1 = M2 = M3 = 5$. First, the 4 tiles in (b) attach one by one to the hollow shape. The filler gadget in (c) can then attach and flood the inside of the shape.

temperature needed.

Finally, extending replication to work in a planar fashion is an open question, as the current construction requires a large assembly to “pop” out of an encased frame. Planar replication systems might provide insight into extending replication into 3D, while maintaining a *spatial* construction.

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